

A Unified Uncertainty based Approach for Optimal Quality Decisions

Dr Jody Muelaner

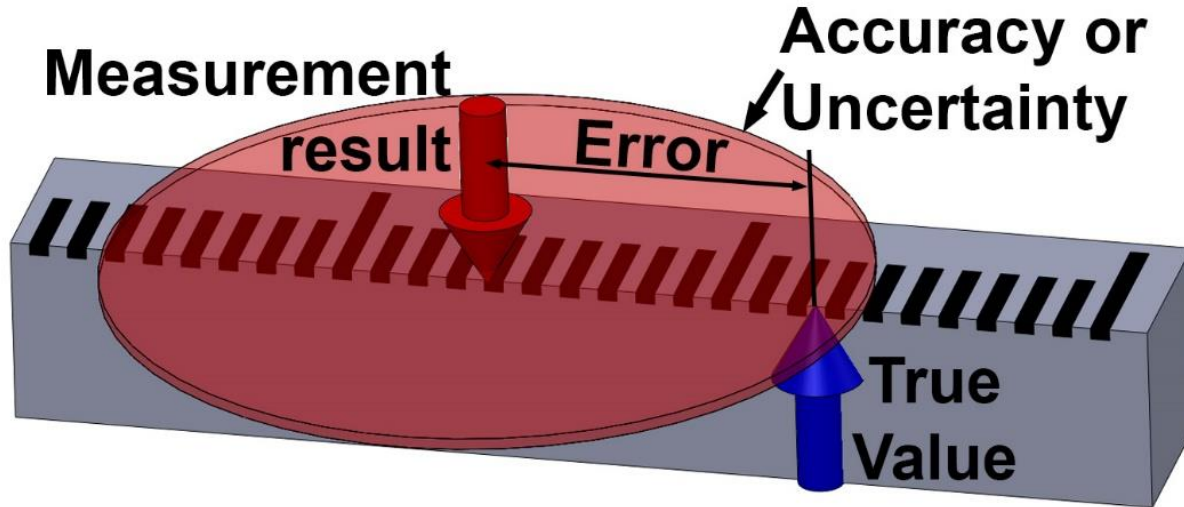
For quality we must understand uncertainty

☹️ But we don't understand how to apply uncertainty to manufacturing... and GUM hasn't been adopted

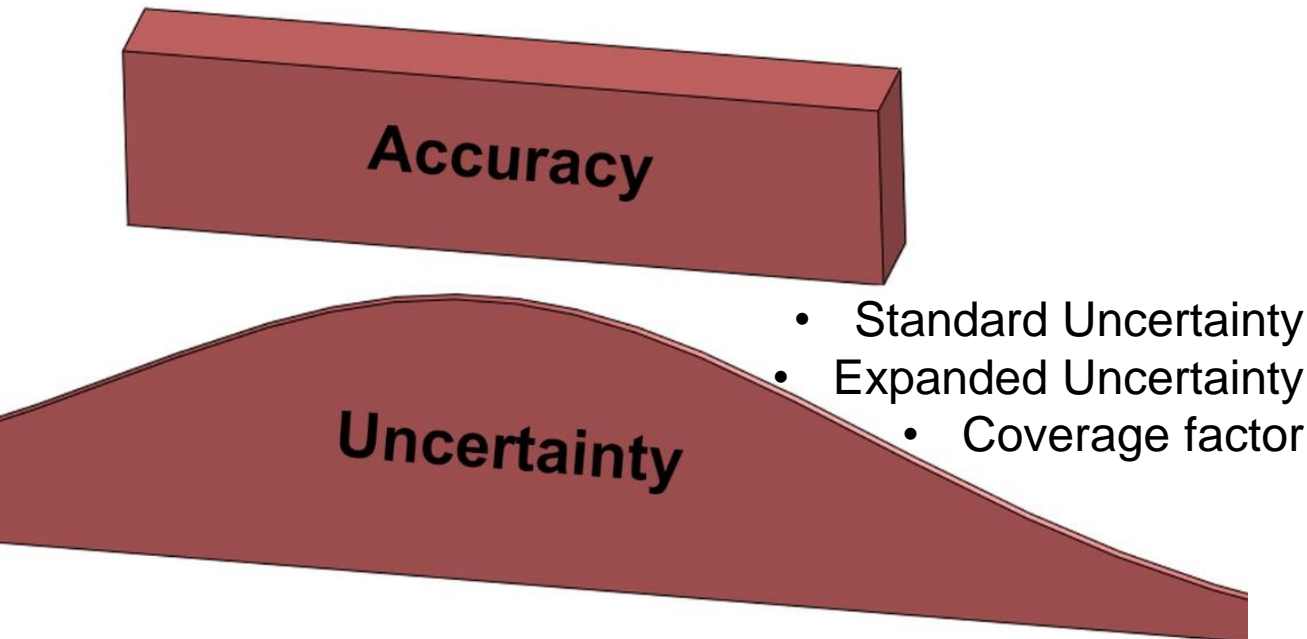
Problem

- Different methods and terms for equivalent quantities
- No single system is fit for purpose
- Arbitrary targets like 'Six-Sigma' are not optimal





True value somewhere in this range



Similar terms:

- Error source: **MSA**
- Influence quantity: **Uncertainty**
- Factor: **SPC**

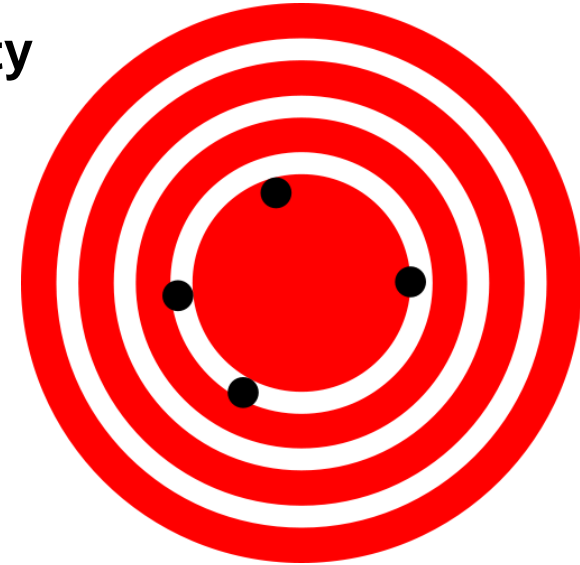
- Random effects / Random uncertainty: **Uncertainty**
- Random error / Precision: **MSA**
- Common causes: **SPC** (was chance causes)

Repeatability

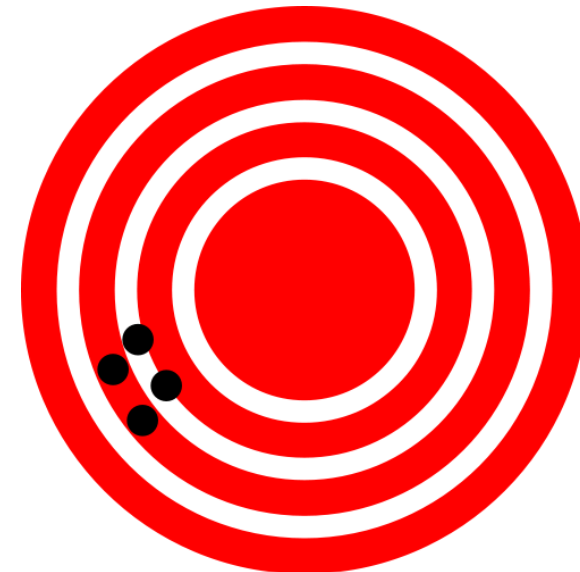
(Short-term variability in SPC)

Reproducibility

(Long-term variability in SPC)



- Bias & Trueness: **MSA**
- Systematic effects: **Uncertainty**
 - Caused by *Influence quantities*
- Special cause variation: **SPC**
 - Was assignable cause
 - When all compensated, so negligible special cause variation, process is in *Statistical Control*: **SPC** (was Stable process)



MSA



Factory measurements



Gauge studies often underestimate reproducibility conditions



Ignores some systematic effects

SPC



Factory processes



Ignores covariance between process and measurement, may hide errors!



May overestimate variation due to MSA for measurements



Tests for 'in-control' differ in sensitivity

GUM Uncertainty



Calibration labs



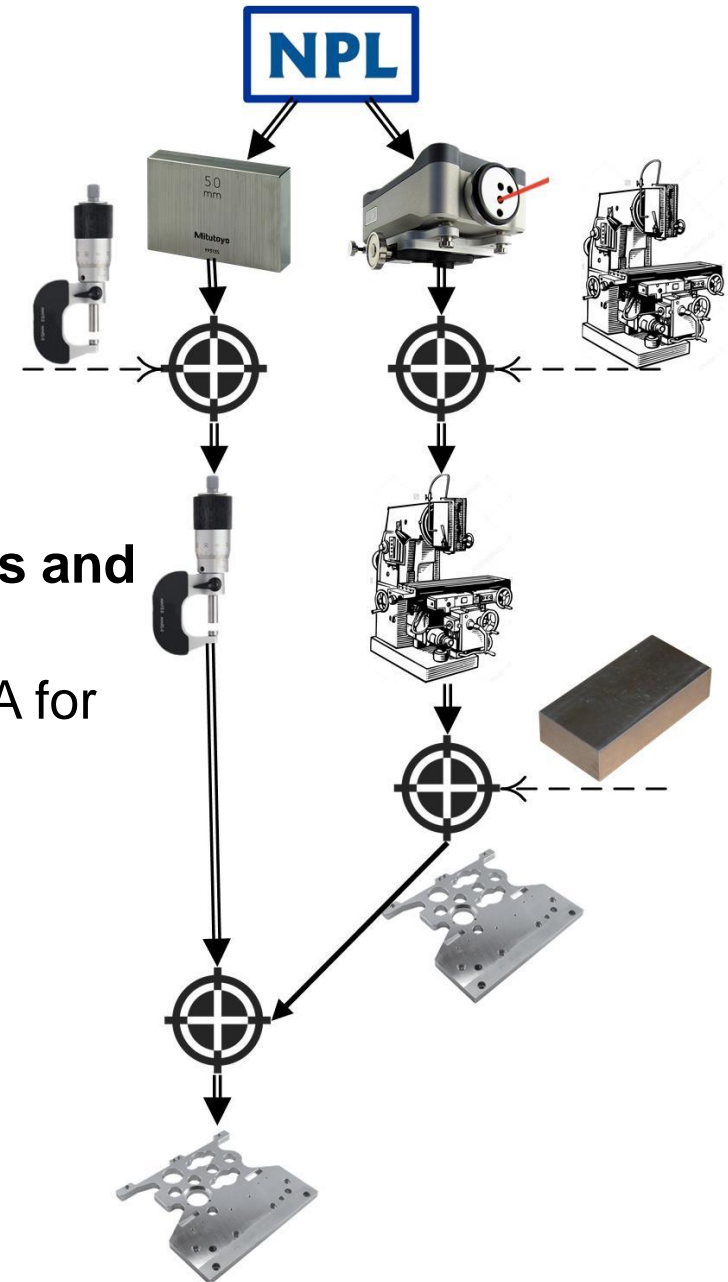
After-the-fact only



Assumptions often not valid



Needs mathematical model



- Gage R&R study often seen as ‘truth’ in industry
- But reproducibility often limited to part and operator!
- Environmental and material property variations often not represented
- GUM approach forces us to consider effect of all influences

- Consider a steel gage measuring a part produced on a steel machine
- Temperature varies
- Expansion of machine and gage cancel
- Significant variation may not appear in SPC data

$$L_{M(T+\Delta T)} = L + \Delta T L \alpha_M$$

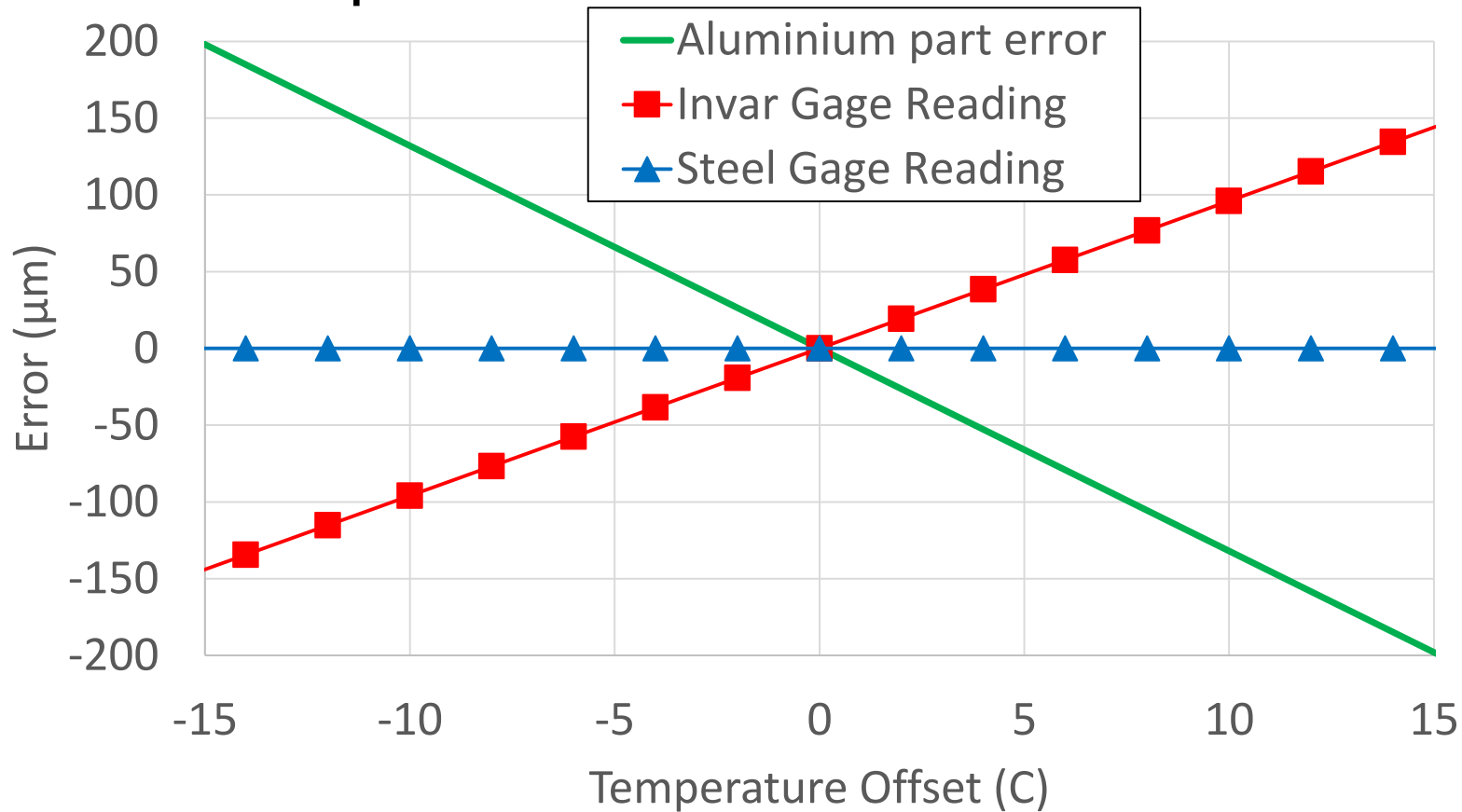
$$L_{P(T)} = L_{M(T+\Delta T)} - \Delta T L \alpha_P$$

$$L_{P(T)} = L + \Delta T L (\alpha_M - \alpha_P)$$

$$L_G = L_{M(T+\Delta T)} - \Delta T L \alpha_G$$

$$L_G = L + \Delta T L (\alpha_M - \alpha_G)$$

Part produced on steel machine tool:



An uncertainty evaluation (GUM) approach would identify that the gage is not capable, but normally MSA is used which can easily miss this effect.

- GUM is ‘after-the-fact’
i.e. correction values
must already be known
to evaluate uncertainty
- GUM assumes Gaussian
output which is only
exact for linear models
- I will use correction for
thermal expansion to
gives examples of these
issues

$$\Delta L = \alpha \Delta T L_0$$

- Linear assumption is
valid
- Typical uncertainties
(95%)
 - α : 6% to 10%
 - ΔT : 0.1 °C to 0.5 °C
 - L_0 : Typically
negligible
- Often significant and
sometimes dominant

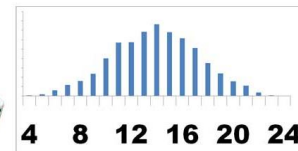
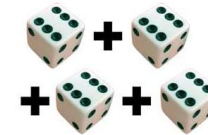
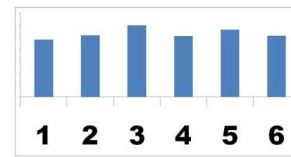
$$\Delta L = \alpha \Delta T L_0$$

$$u_{\Delta L}^2 \approx (\alpha \Delta T u_L)^2 + (L \Delta T u_\alpha)^2 + (L \alpha u_T)^2$$

- GUM assumes each input quantity has been determined
- We often need uncertainty before they are determined
 - Estimate uncertainty for a planned measurement
 - Determine probability of parts conforming
- Two approaches typically used
 - If uncertainty in the input has negligible effect use nominal value
 - If it is significant use worst case value
- Why use worst case?
 - Because GUM doesn't have a solution!
- Modelling this is easy if we consider errors and propagate the uncertainty in these errors with MCS

$$\Delta L = \alpha \Delta T L_0$$

$$u_{TE}^2 \approx (\alpha \Delta T u_L)^2 + (L \Delta T u_\alpha)^2 + (L \alpha u_T)^2 \\ + (\Delta T u_L u_\alpha)^2 + (\alpha u_L u_T)^2 + (L u_\alpha u_T)^2 \\ + (u_T u_L u_\alpha)^2$$

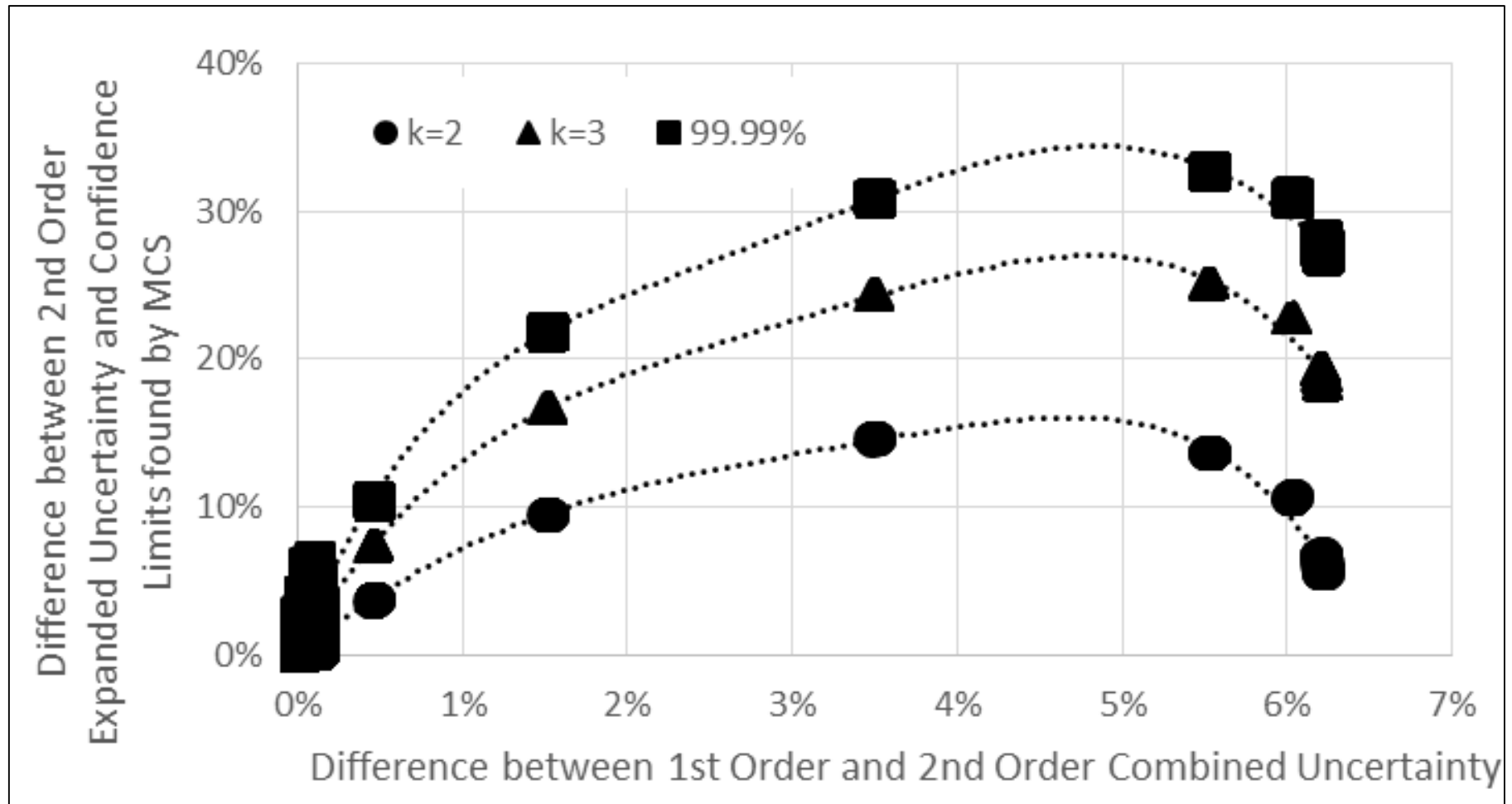


- Terms evaluated for 14400 combinations of parameters:
 - Lengths between 1 μm and 100 m
 - Fractional standard uncertainty in length of between 10^{-7} and 10^{-3}
 - CTE's between 1.2 and 23 ppm/ $^{\circ}\text{C}$
 - Fractional standard uncertainty in CTE of between 0.2% and 37%
 - Temperature offsets of between 0.01 $^{\circ}\text{C}$ and 20 $^{\circ}\text{C}$
 - Fractional standard uncertainty in measurement of the temperature offset of between 0.001 $^{\circ}\text{C}$ and 2 $^{\circ}\text{C}$.

$$\Delta L = \alpha \Delta T L_0$$

$$\begin{aligned} u_{TE}^2 \approx & (\alpha \Delta T u_L)^2 + (L \Delta T u_\alpha)^2 + (L \alpha u_T)^2 \\ & + \cancel{(\Delta T u_L u_\alpha)^2} + \cancel{(\alpha u_L u_T)^2} + (L u_\alpha u_T)^2 \\ & + \cancel{(u_T u_L u_\alpha)^2} \end{aligned}$$

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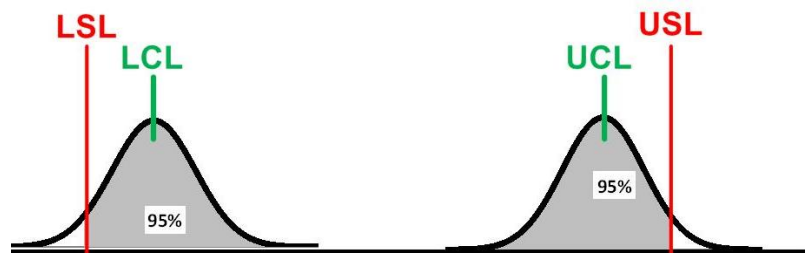


A part meets 1 of 4 conditions,
with finite probabilities:

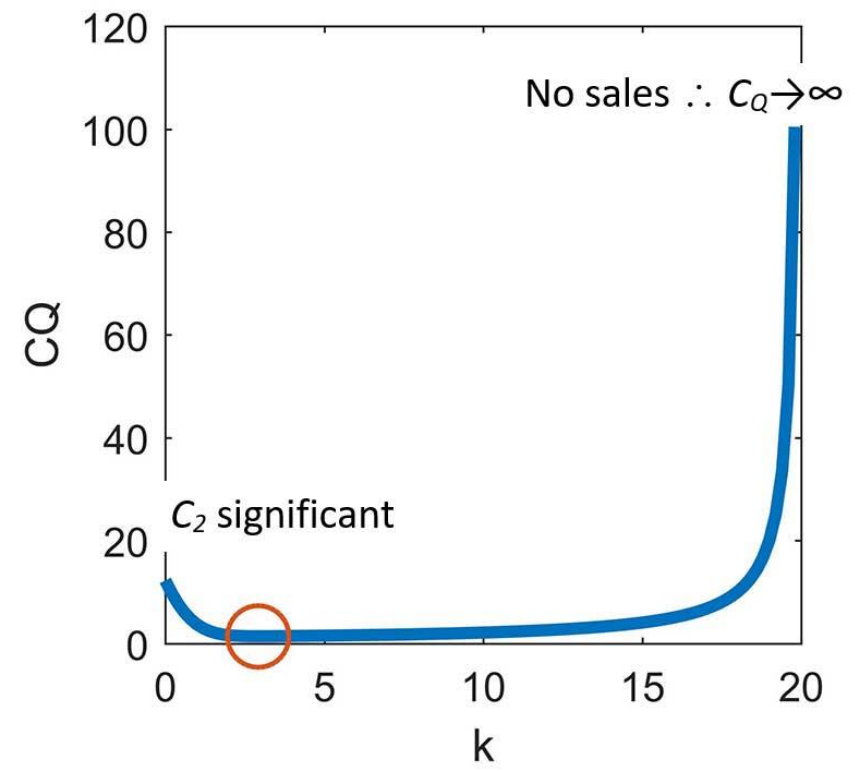
	Pass Verification	Fail Verification
In-Spec'	True Negative, P_1	False Positive, P_3
Out-of-Spec'	False Negative, P_4	True Positive, P_2

- Cost of manufacture (C_1) occurs for every part
- Defects reaching customer have additional cost (C_2)

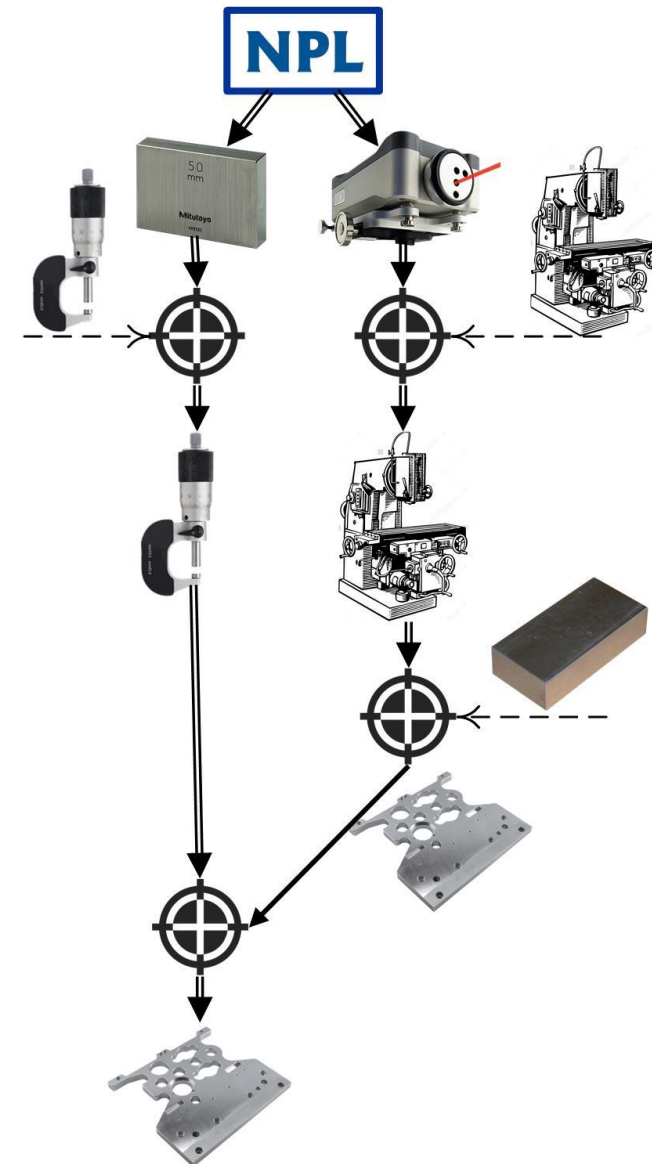
$$C_Q = \frac{C_1 + P_4 C_2}{P_1 + P_4} \quad \begin{matrix} M = U/T \\ P = \sigma/T \\ k \end{matrix}$$



1. M and P discrete values (instruments and machines). Try all combos
2. Find k to minimize C_Q for each combination (PS using MVN CDF)



- Cost based optimization algorithms
 - Process selection
 - Instrument selection
 - Set of conformance limits
- Standardised terminology
- Uncertainty evaluation algorithms
 - Generic models of influences
 - Before-the-fact uncertainty
 - Non-Gaussian distributions
- Algorithms for experimentally verifying uncertainty models



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